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**United States Patent** [19]

Endo et al.

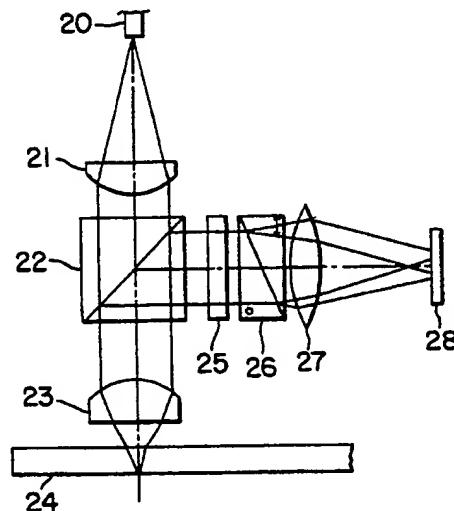
[11] **Patent Number:** 5,416,755[45] **Date of Patent:** May 16, 1995[54] **OPTICAL PICKUP USING SPLIT BEAMS  
IMPINGING ON DIFFERENT  
PHOTO-DETECTOR AREAS**[75] **Inventors:** Kiyonobu Endo; Kazuya Matsumoto; Tetsuro Kuwayama, all of Yokohama, Japan[73] **Assignee:** Canon Kabushiki Kaisha, Tokyo, Japan[21] **Appl. No.:** 195,882[22] **Filed:** Feb. 4, 1994**Related U.S. Application Data**

[60] Continuation of Ser. No. 954,047, Sep. 30, 1992, abandoned, which is a division of Ser. No. 658,428, Feb. 20, 1991, abandoned, which is a continuation of Ser. No. 349,963, May 8, 1989, abandoned, which is a continuation of Ser. No. 832,651, Feb. 25, 1986, abandoned.

[30] **Foreign Application Priority Data**Feb. 28, 1985 [JP] Japan ..... 60-039050  
Feb. 28, 1985 [JP] Japan ..... 60-039051  
Apr. 8, 1985 [JP] Japan ..... 60-072733[51] **Int. Cl.6** ..... G11B 11/00  
[52] **U.S. Cl.** ..... 369/13; 369/11C;  
369/44.38; 360/114[58] **Field of Search** ..... 369/13, 14, 44.39, 44.15,  
369/47, 110, 112, 120, 118, 109, 44.23, 44.37,  
44.38, 44.24, 44.12, 44.11; 360/114, 59; 365/12,  
122; 250/201.2[56] **References Cited****U.S. PATENT DOCUMENTS**4,513,408 4/1985 Nomura et al. ..... 369/46  
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4,626,679 12/1986 Kuwayama et al. ..... 250/227.11  
4,676,623 6/1987 Akashi et al. ..... 250/578**FOREIGN PATENT DOCUMENTS**57-44241 3/1982 Japan .  
0088540 6/1982 Japan .  
59-77649 5/1984 Japan .  
59-203259 11/1984 Japan .*Primary Examiner*—Georgia Y. Epps*Assistant Examiner*—Ali Neyzari*Attorney, Agent, or Firm*—Fitzpatrick, Cella, Harper & Scinto[57] **ABSTRACT**

An optical pickup device for producing information magnetically recorded on a recording medium includes a light source for generating a light beam polarized in a predetermined direction. An object lens is provided for focusing the light beam generated from the light source onto the recording medium. A beam splitter is arranged in an optical path extending from the light source to the recording medium, the beam splitter having a reflection plane for reflecting the light beam from the light source toward the recording medium. The beam splitter simultaneously causes the reflecting light from the recording medium to pass through the reflection plane to separate the reflected light beam from the light beam irradiated toward the recording medium. The polarization state of the reflecting light beam is modulated in accordance with the recorded information. The beam splitter splits the reflected light beam passed through the reflection plane into first and second light beams both of which are polarized in directions perpendicular to each other. The beam splitter has a bi-refractive property. First and second detection circuits are also provided for detecting the first and second light beams, respectively, and for providing first and second detection outputs respectively corresponding thereto. Circuitry is also provided for differentiating the detection outputs from the first and second detection circuits to provide information signals.

4 Claims, 11 Drawing Sheets



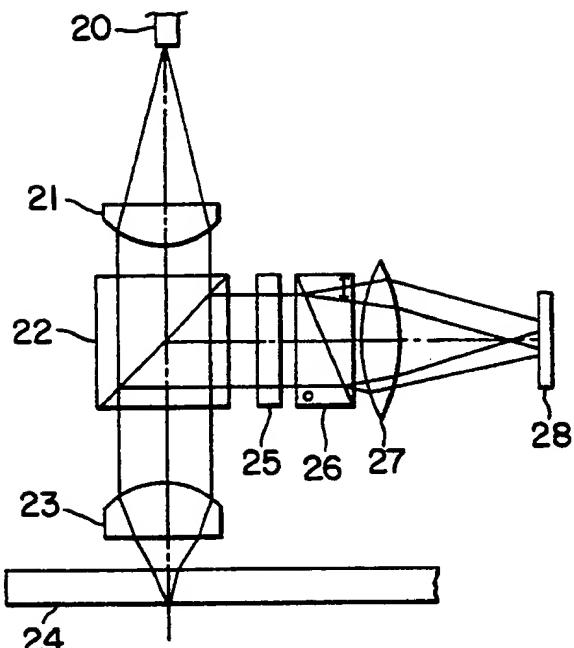


FIG. 1A

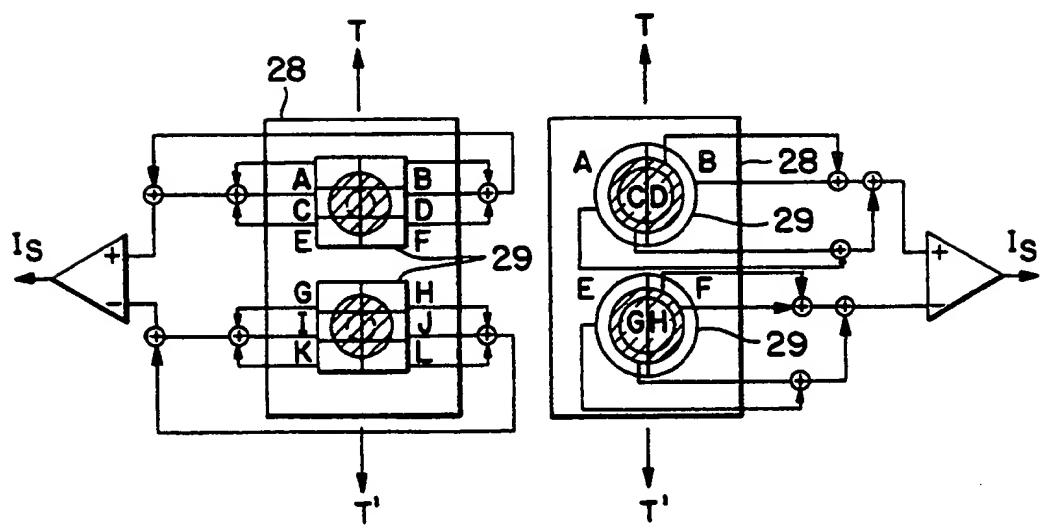


FIG. 1B

FIG. 1C

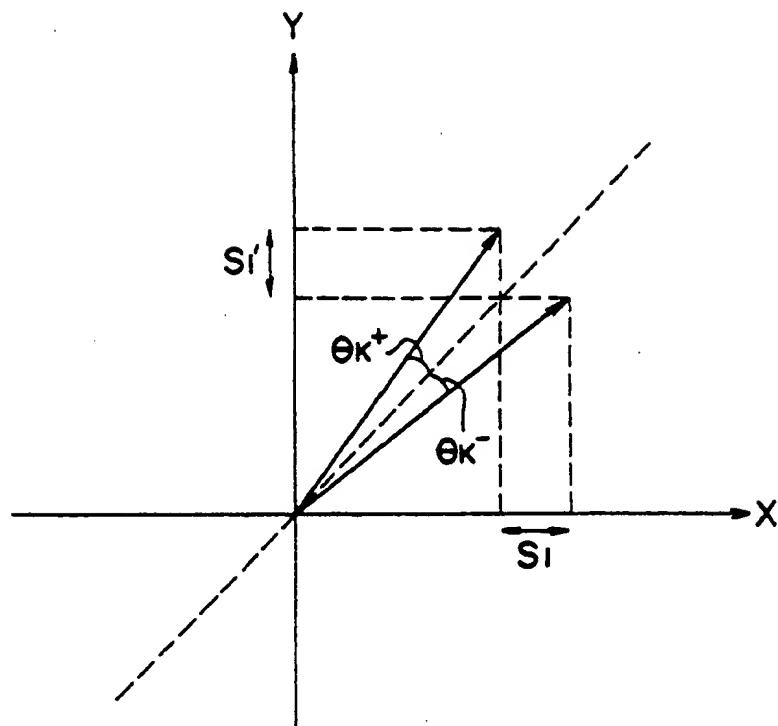


FIG. 2

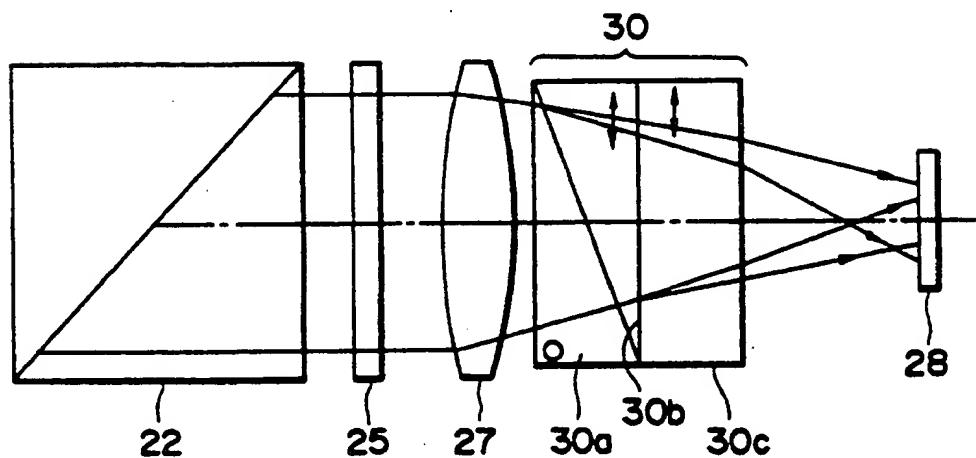
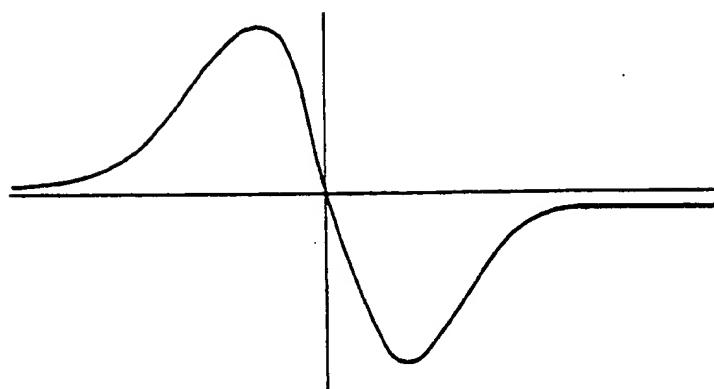
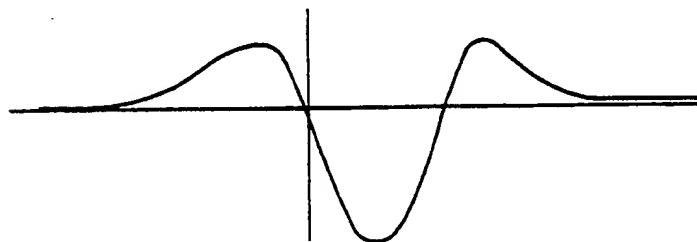
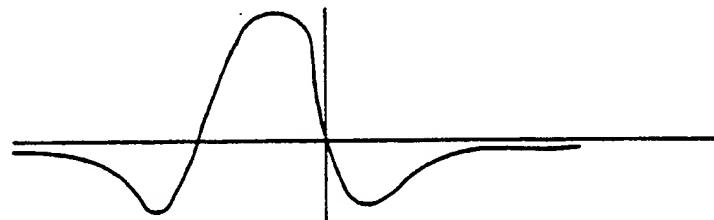
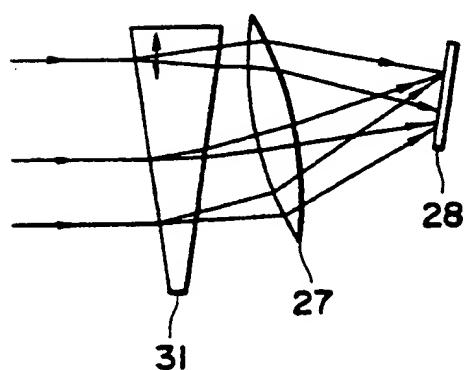
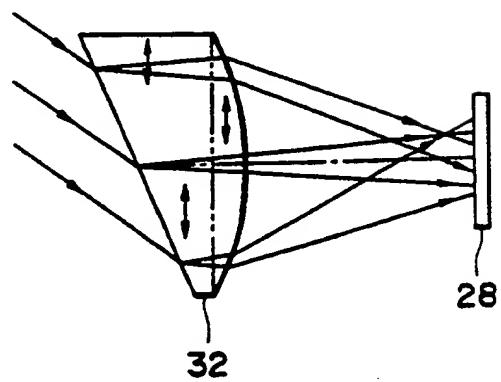


FIG. 3

**FIG. 4A****FIG. 4B****FIG. 4C****FIG. 5****FIG. 6**

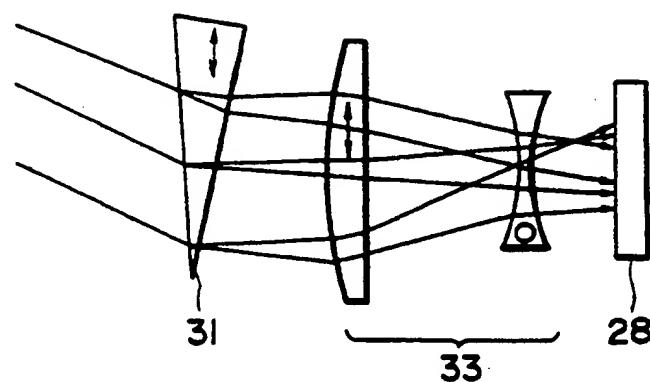


FIG. 7

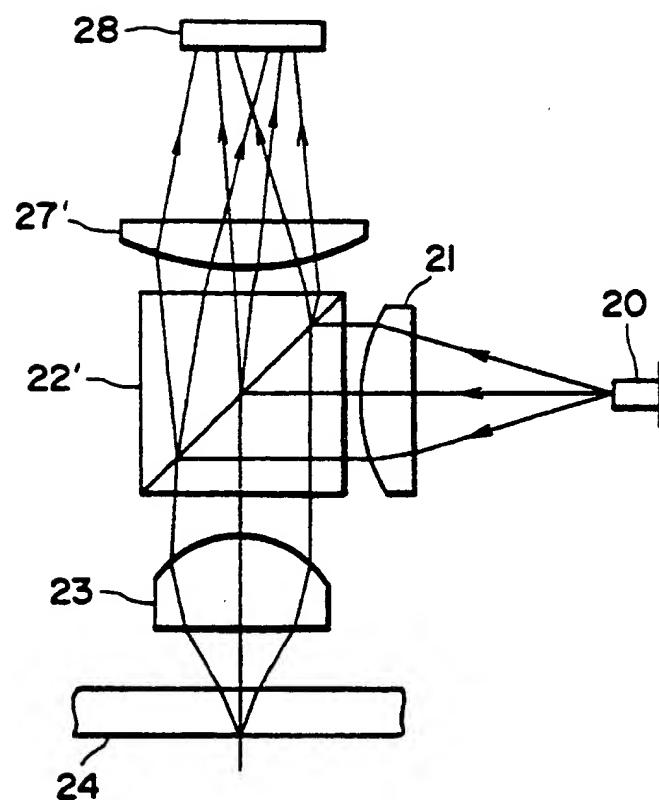


FIG. 8

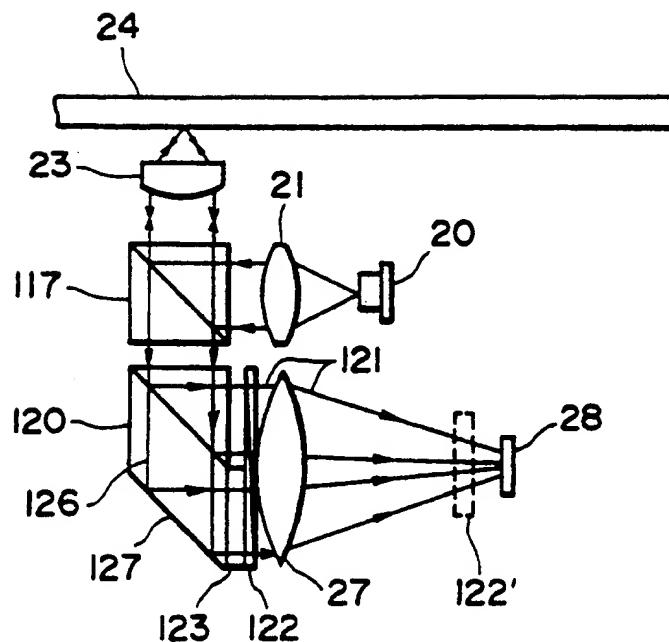


FIG. 9

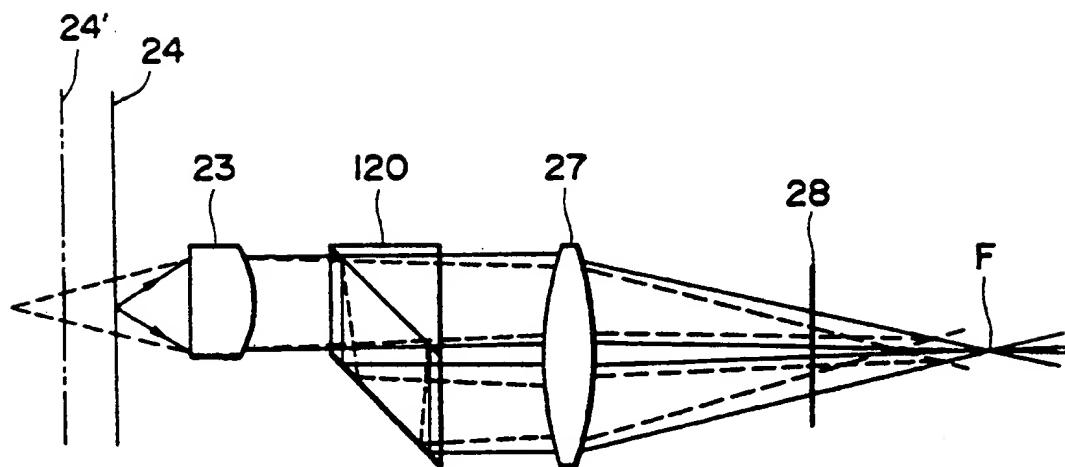


FIG. 10

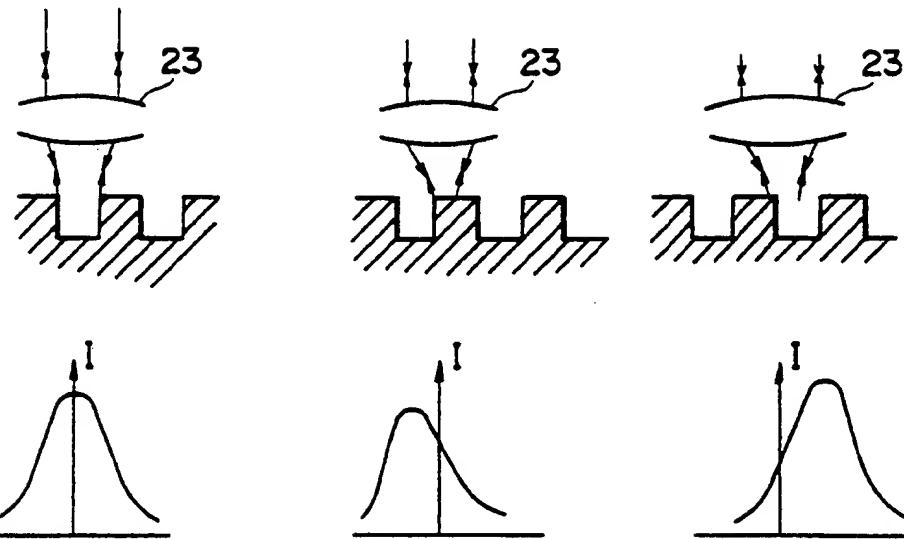


FIG. II A

FIG. II B

FIG. II C

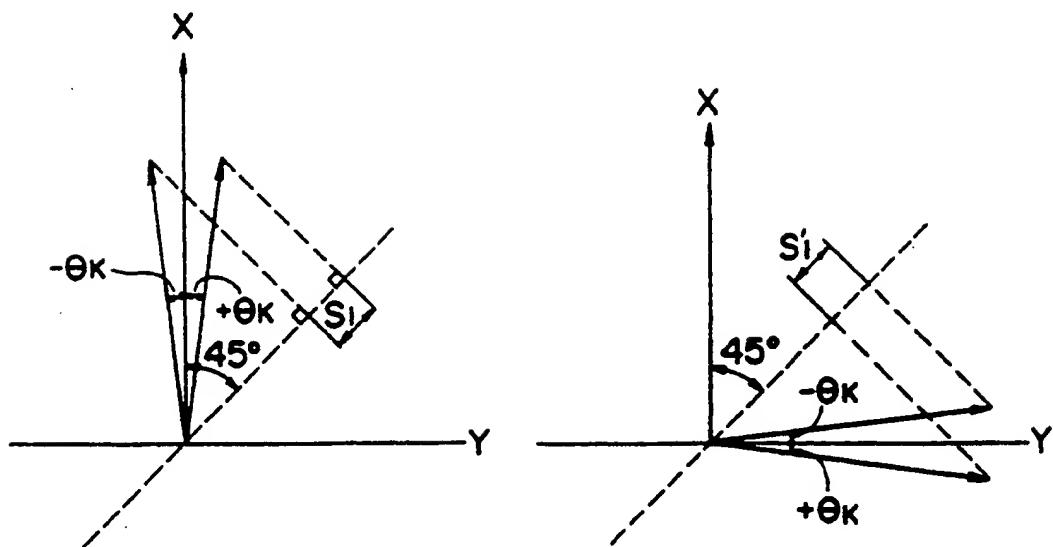


FIG. 12A

FIG. 12B

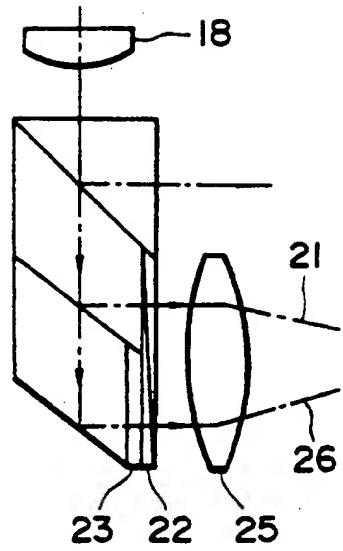


FIG. 13

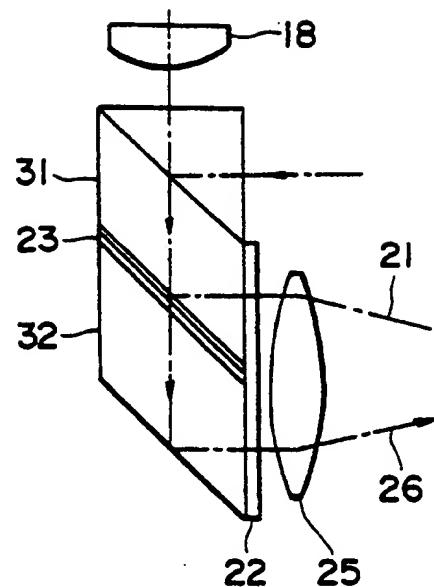


FIG. 14

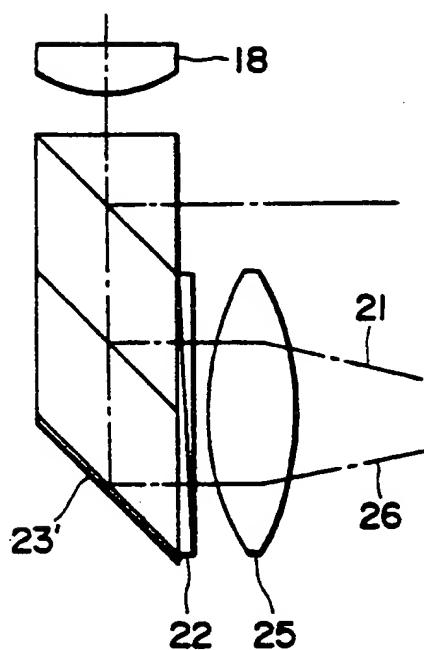


FIG. 15

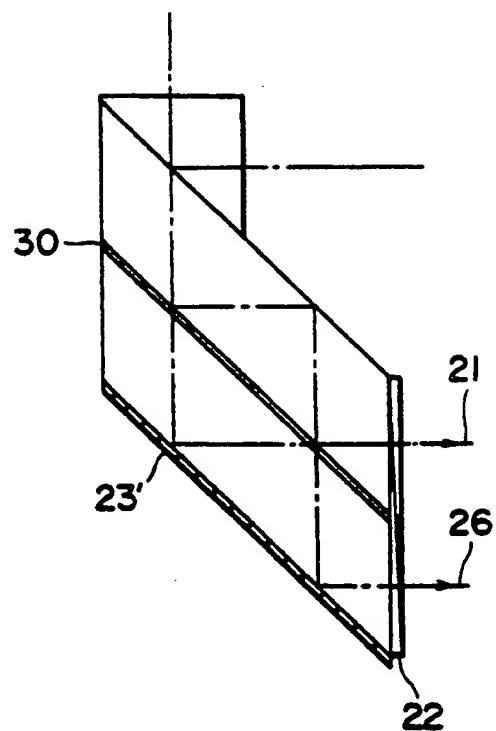


FIG. 16

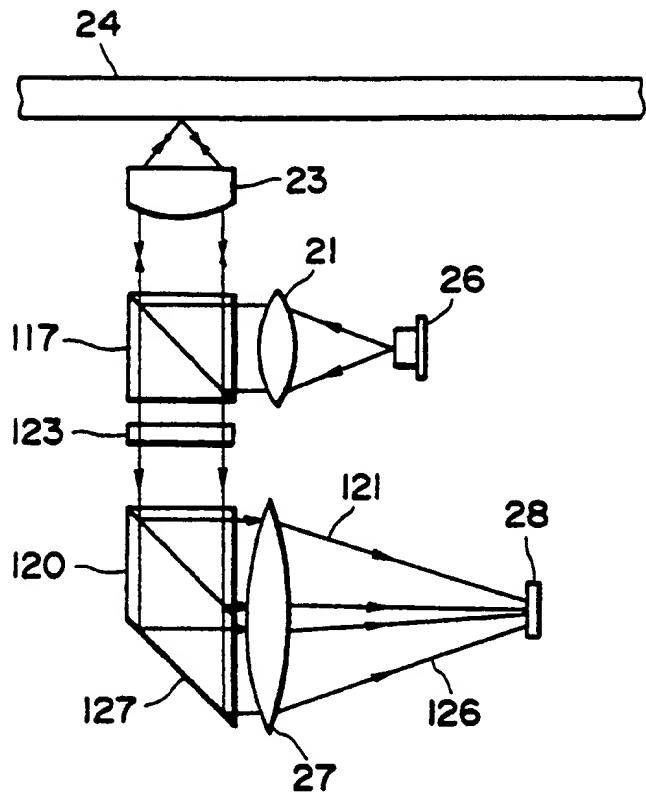
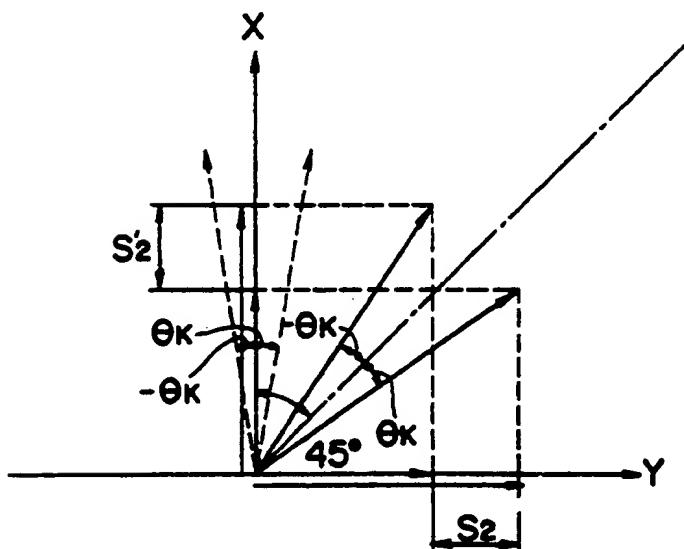


FIG. 17



## FIG. 18

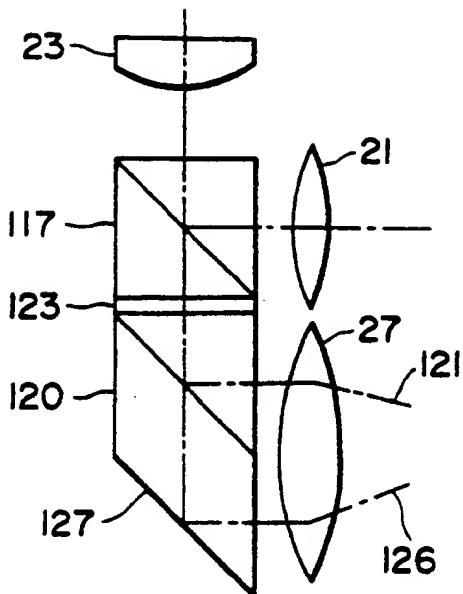


FIG. 19

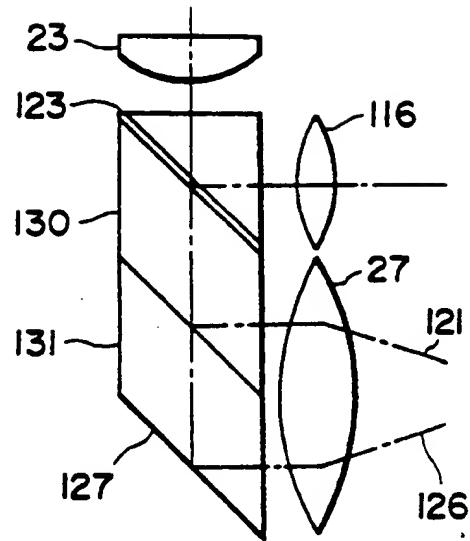


FIG. 20

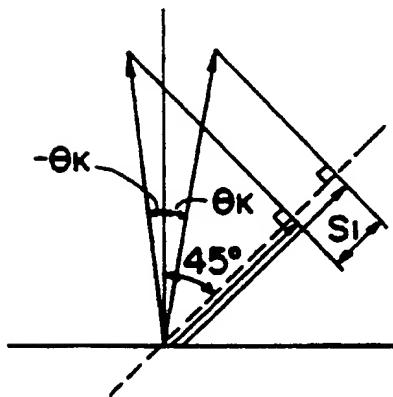


FIG. 21A

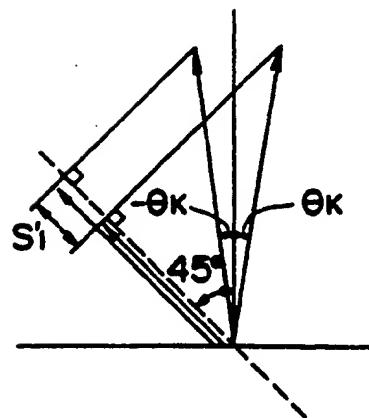


FIG. 21B

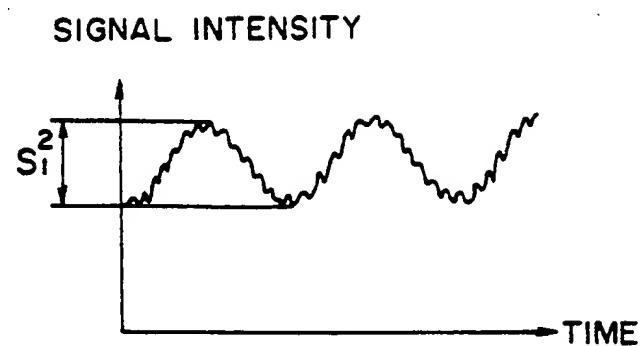


FIG. 22A

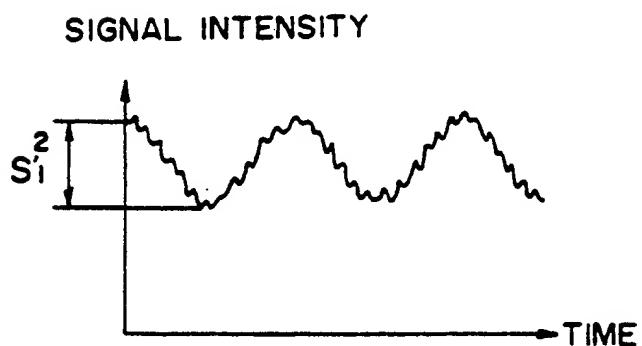


FIG. 22B

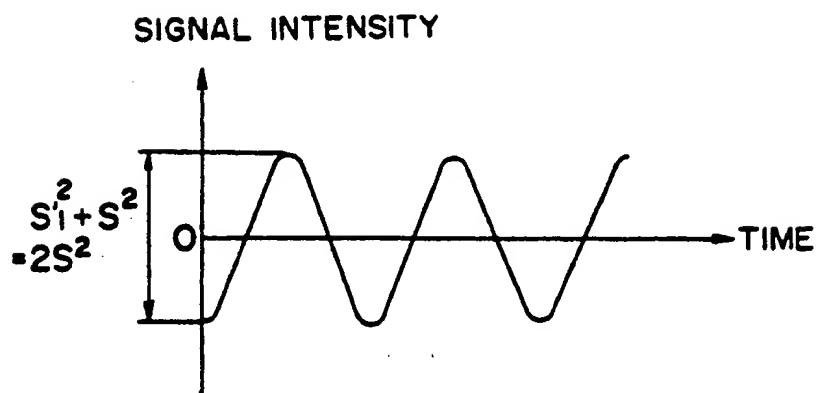


FIG. 22C

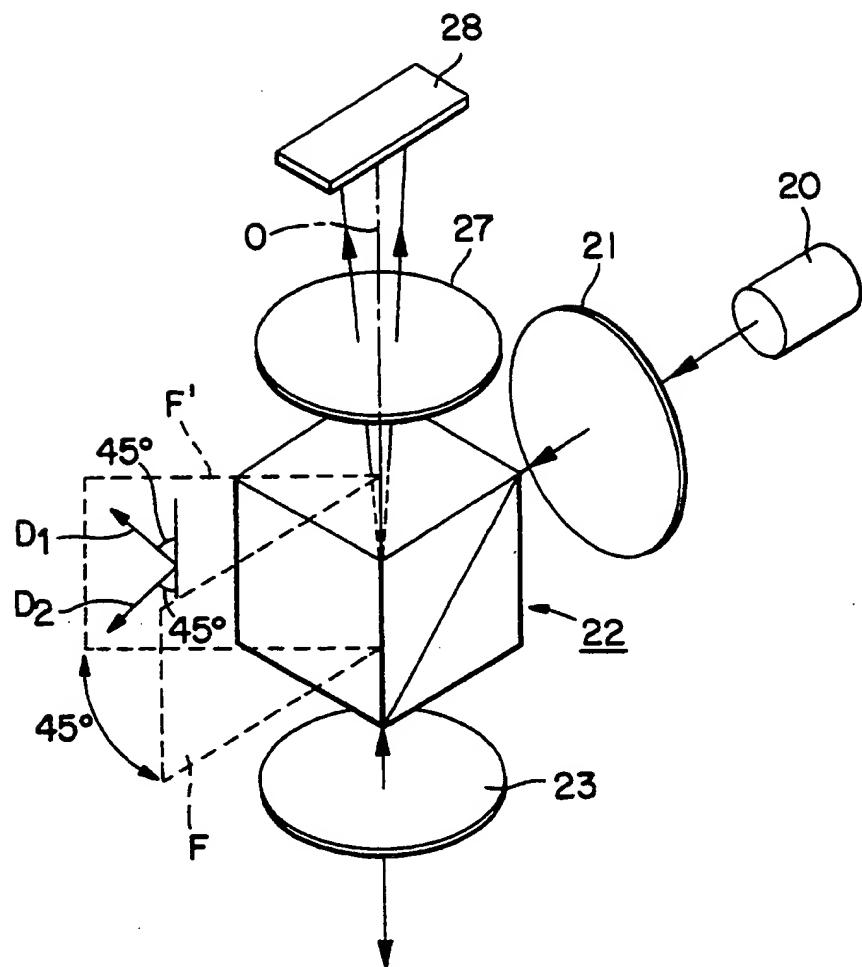


FIG. 23

**OPTICAL PICKUP USING SPLIT BEAMS  
IMPINGING ON DIFFERENT PHOTO-DETECTOR  
AREAS**

This application is a continuation of application Ser. No. 07/954,047, filed Sep. 30, 1992, which is a division of application Ser. No. 07/658,428, filed Feb. 20, 1991, which is a continuation of application Ser. No. 07/349,963, filed May 8, 1989, which is a continuation of application Ser. No. 06/832,651, filed Feb. 25, 1986, all now abandoned.

**BACKGROUND OF THE INVENTION**

1. Field of the Invention

The present invention relates to an optical pickup for irradiating a light beam on an information recording area of an information carrier to detect or record information, and more particularly to a compact, low cost optical pickup capable of reproducing a signal at a high S/N ratio.

2. Related Background Art

Research and development for a writable optical disk recording medium and an optical disk recording and reproducing apparatus have been vigorously prosecuted.

Examples of such apparatus are shown in U.S. Pat. No. 4,451,863 and IBM Technical Disclosure Bulletin Vol. 19, No. 4, issued September 1976.

However, such a prior art optical pickup has many parts and is disadvantageous as regards reduction in a size and cost. Further, a plurality of photo-detectors must be accurately positioned and adjustment thereof is troublesome.

**SUMMARY OF THE INVENTION**

It is an object of the present invention to provide an optical pickup which is compact and easy to adjust optically.

An optical pickup apparatus according to the present invention includes photodetection means having a plurality of detection areas. Means are provided for converting, into an electrical signal, a light beam emitted from a recording medium on which information is magnetically recorded and modulated in intensity. These means also split the light beam into two beams and guide them respectively to different areas of the photodetection means. Means are also provided for processing outputs from each of the areas of the photodetection means to provide an information signal.

**BRIEF DESCRIPTION OF THE DRAWINGS**

FIG. 1A shows a first embodiment of an optical pickup of the present invention.

FIGS. 1B and 1C show enlarged views of photo-detectors used in the pickup of FIG. 1A.

FIG. 2 shows a signal amplitude components of a light beam.

FIG. 3 shows a modification of the first embodiment of the present invention.

FIG. 4, consisting of FIGS. 4A, 4B and 4C, shows focus error signals.

FIGS. 5, 6, 7 and 8 show other modifications of the first embodiment of the present invention.

FIG. 9 shows a second embodiment of the optical pickup of the present invention.

FIG. 10 illustrates a principle of detection of an AF signal by the present invention.

FIG. 11, consisting of FIGS. 11A, 11B and 11C, illustrates a principle of detection of an AT signal by the present invention,

FIG. 12, consisting of FIGS. 12A and 12B, illustrates a principle of detection of an information signal by the present invention,

FIGS. 13, 14, 15 and 16 show modification of the second embodiment of the optical pickup shown in FIG. 9,

FIG. 17 shows a third embodiment of the optical pickup of the present invention,

FIG. 18 illustrates a principle of detection of the information signal by the present invention,

FIGS. 19 and 20 show modifications of the optical pickup of FIG. 17,

FIGS. 21 (consisting of FIGS. 21A and 21B) and 22 (consisting of FIGS. 22A, 22B and 22C) illustrate principles of differential detection, and FIG. 23 is a perspective view of prism 22.

**DESCRIPTION OF THE PREFERRED  
EMBODIMENTS**

FIG. 1A shows a first embodiment of an optical pickup according to the present invention. A light beam emitted from an LD 20 is collimated by a collimating lens 21, passes through a beam splitter 22 and is focused by an object lens 23 to a fine spot on a recording medium 24. A reflected light beam from the recording medium 24 again passes through an object lens 23, is reflected by the beam splitter 22, passes through a half-wave plate 25 with the direction of its plane of polarization being rotated by 45 degrees, and is directed to a Wollaston prism 26. As a result, the light beam is split into a linearly polarized light beam which vibrates in the plane of the drawing and a linearly polarized light beam which vibrates in a plane normal to that of the drawing; and both of the split beams are condensed by a sensor lens 27.

FIGS. 1B and 1C show examples of split portions or areas of a photo-sensor of a photo-detector 28. When the object lens 23 and the recording medium 24 are in an in-focus position, the light beam spreads to the hatched areas shown in FIGS. 1B and 1C. Signal outputs  $I_A$ ,  $I_B$ ,  $I_C$ ,  $I_D$ ,  $I_E$ , and  $I_F$ , from the photo-sensors A-F, respectively, and a focus error signal  $I_{AF1}$ , have the following relationship.

$$I_{AF1} = (I_A + I_B + I_E + I_F) - (I_C + I_D)$$

In FIG. 1B, if the recording medium 24 moves away from the object lens 23, the light spot becomes smaller, as shown by a broken line in FIG. 1B. As a result, the outputs  $I_C$  and  $I_D$  increase and the focus error signal  $I_{AF1}$  becomes negative. When the recording medium 24 moves nearer to the lens 23, the light spot on the photo-sensor 29 becomes larger and the focus error signal  $I_{AF1}$  becomes positive.

Where the concentric photo-sensors 29 shown in FIG. 1C are employed, a difference between the outer photo-sensor and the inner photo-sensor is used so that the focus error signal is detected in a similar manner.

On the other hand, a tracking error signal may be detected in the present invention by a known push-pull method, like that shown in U.S. Pat. No. 3,931,459. The tracking error signal may be detected by calculating

$$I_{AT1} = (I_A + I_C + I_E) - (I_B + I_D + I_F)$$

A principle of differential detection of the opto-magnetic information signal by the optical pickup of the present invention is now explained.

In FIG. 1A, the reflected light from the recording medium 24 is directed to the half-wavelength plate 25 with the polarization plane thereof being rotated through an angle  $\theta_K$  or  $-\theta_K$  by the magnetic pattern of the recording medium 24 (direction of magnetization is either upward or downward) by the magneto-optical effect. The half-wavelength plate 25 has a crystal axis arranged at  $22.5^\circ$  with respect to a crystal axis of the Wollaston prism 26. Since the Wollaston prism 26 splits the reflected light beam into two linearly polarized light beams having vibration planes orthogonal to each other, those light beams are detected by the photo-sensor 28 as signals of opposite phases, as shown in FIG. 2.

In FIG. 2, the X axis represents a compound of the crystal axis of a first prism of the Wollaston prism 26 and the Y axis represents a component normal thereto. The light beam rotated by  $\theta_K$  or  $-\theta_K$  from the polarization plane of the reflected light beam by the magneto-optical effect (a broken line in FIG. 2 shows the polarization plane) has its polarization plane rotated by  $45^\circ$  by the half-wavelength plate 25. Since it is thereafter divided in two by the Wollaston prism 26, the resulting light beams have an equal variation amplitude (S1 and S1') and opposite phases. By detecting those two light beams by means of the photo-sensors 29, the opto-magnetic signal of the recording medium 24 can be produced. In the photo-detector 28 of FIG. 1B, the opto-magnetic information signal  $I_S$  is given by

$$I_S = (I_A + I_B + I_C + I_D + I_E + I_F) - (I_G + I_H + I_I + I_K + I_L)$$

and in the photo-detector 28 of FIG. 1C, it is given by

$$I_S = (I_A + I_B + I_C + I_D) - (I_E + I_F + I_G + I_H)$$

In accordance with the present embodiment, the size and weight of the apparatus are reduced and the reliability is improved. Since a set of photo-sensors 29 which differentially detect the light beams are arranged on one substrate, the photo-detector 28 is insensitive to external changes such as a change of environmental temperature.

By arranging a set of amplifiers on the same substrate as the photo-detectors, the frequency characteristics and temperature characteristics of those circuits are well matched and signal quality is further improved. By incorporating the differential amplifier for differentially detecting the signals in the photo-detector, noise-resistant detection is attained.

A modification of the first embodiment of the present invention is shown in FIG. 3. The light beam reflected by the beam splitter 22 and transmitted through the half-wave plate 25 (optical elements in front of the beam splitter 22 are omitted in FIG. 3) is condensed by a condenser lens 27, and the condensed beam is directed to a polarization/separation element 30 comprising two prisms 30a and 30b having crystal axes orthogonal to each other (which form a Wollaston prism) and a polarization plate 30c having the same crystal axis as that of the prism 30b. The light beam transmitted through the polarization/separation element 30 propagates in different directions for an ordinary ray and an extraordinary ray, and an equivalent optical thickness changes with a difference between refractive indices  $N_o$  and  $N_e$  for the ordinary ray and the extraordinary ray. Accordingly,

focusing positions for the ordinary ray and extraordinary ray are different. Thus, the photo-sensor 29 of the photo-detector 28 is arranged at an unfocused position for the light beam of one polarization direction and in the diverging light beam after focusing for the other light beam.

FIG. 4A shows a focus error signal produced in FIG. 3. FIGS. 4B and 4C show focus error signals produced by a single concentric circular photo-detector. They have undesirable side peaks to an ideal S-curve. In the embodiment of FIG. 3 which uses the combination of converging and diverging photo-detectors, the undesired peak is eliminated as shown in FIG. 4A and a desirable S-shaped focus error signal is produced. In FIG. 3, an interval between the two light spots on the photo-detector 28 can be finely adjusted by moving the Wollaston prism (30a and 30b) back and forth.

Another modification of the first embodiment of the present invention is shown in FIG. 5. The light beam from the beam splitter (not shown in FIG. 5) is separated into an ordinary ray and an extraordinary ray by a prism 31 formed of crystal and is focused onto the photo-detector 28 by the focusing lens 27. The photo-detector 28 may be arranged obliquely to the light beam by an appropriate angle.

Not only the prism but also the focusing lens 27 may be manufactured of crystal. FIG. 6 shows an example thereof. An optical element 32 has a prism on one side and a lens on the other side. As a result, converging and diverging light beams separated in accordance with the polarization status of the incident light are directed to the photo-detector 28.

FIG. 7 shows a modification in which the focusing lens 27 is substituted by a teletype telescopic lens 33. With this arrangement, the light beams necessary for the differential direction are finely separated.

The above embodiment and modifications may be implemented by optical medium which form a beam splitter 22' as shown in FIG. 8.

In FIG. 8, the light beam from the laser 20 is collimating by the collimating lens 21 and reflected by a reflection plane of the beam splitter 22'. The incident light beam is a perfectly linearly polarized beam, and there is no difference in the effect whether the optical medium of the beam splitter 22' is isotropic, such as glass, or bi-refractive, such as quartz. The light beam reflected by the opto-magnetic medium 24 again passes through the beam splitter 22'. If the beam splitter 22 is made of a uniaxial crystal having a crystal axis appropriately oriented, the light beam is separated into two linearly polarized beams, which are directed to the sensor 28 through a sensor lens 27' and are differentially detected thereby. The crystal axis may form an angle of  $45^\circ$  to the vertical direction in the drawing and is rotated approximately  $45^\circ$  with respect to the plane of the drawing.

As seen from FIG. 23, the vertical plane which includes an optical axis of a light beam emitted from a light source and an optical axis of a light beam reflected by the opto-magnetic medium, is indicated by reference character F. Since the crystal axis of the prism is rotated by  $45^\circ$  with respect to the virtual plane F, the crystal axis is parallel with a plane (not shown) perpendicular to a plane F', or the plane of the drawing in FIG. 23. The crystal axis may form an angle of  $45^\circ$  to the vertical direction of the drawing in FIG. 8, namely, in the direction of the optical axis zero shown in FIG. 23. Accord-

ingly, the crystal axis of the prism is directed to the direction  $D_1$  or the direction  $D_2$  shown by the arrow in FIG. 23.

While the Wollaston prism or the single prism was shown as means for separating the light beam by the difference between polarization status of the incident light beam, the embodiment of the separation means is not limited thereto but may be a Rochon prism or a Senarmont prism, etc. The crystal parallel plates or convex lens is shown as means for creating a converging or a diverging light beam depending on the difference in polarization status, although that means may instead be a combination of convex and concave telescopic lens or other means.

FIG. 9 shows a second embodiment of the optical pickup of the present invention. The light beam emitted from the LD 20 is collimated by a collimating lens 21, reflected by a first beam splitter 117 and focused by the object lens 23 to a fine spot on the recording medium 24. The reflection light from the recording medium 24 again passes through the object lens 23 and the first beam splitter 117, is directed to a second beam splitter 120 and is split thereby into two light beams. The first split beam 121, reflected by the second beam splitter 120, passes through a polarization element 122 such as a polarization plate and is focused by the focusing lens 27 onto the photo-sensor 28. The same effect may be attained when the polarization element 122 is arranged between the focusing lens 27 and the photo-sensor 28. On the other hand, the second split beam 126, after passing through the second beam splitter 120, is reflected by a reflection area 127 at the bottom of the beam splitter 120, passes through the half-wavelength plate 123 and the polarization element 122, and is focused by the focusing lens 27 onto the photo-sensor 28.

The photo-sensor 28 is arranged at a position spaced from a focal plane on which the split light beams 121 and 126 are focused by the focusing lens 27. The photo-sensor 28 has 12 photo-sensing areas as shown in FIG. 1B.

A principle for detection of the AF and AT signal and the differential detection of the information signal in the apparatus of FIG. 9 is now explained.

FIG. 10 shows the principle of detection of the AF signal. Only those of the elements shown in FIG. 9 which are necessary for the AF detection are shown in FIG. 10. When the recording medium 24 is located on the focal plane of the object lens 23, the light beam is directed as shown by solid lines and focused to a focal point F of the focusing lens 27. When the recording medium moves away from the focal plane of the object lens 23, the light beam is focused at forward side of the optical axis of the focusing lens 27 as shown by broken lines. When the recording medium moves closer from the focal plane of the object lens 23, the light beam is focused beyond the optical axis of the focusing lens 27. Accordingly, when the optical sensor 28 is arranged off the point F, the distribution of the intensity of the split light beams on the optical sensor 28 appears reduced or enlarged on the sensor depending on the position of the recording medium.

Where the photo-sensor 28 has twelve photo-sensing areas, the operation is as follows. The light beam of the photo-sensor in the in-focus state of the object lens 23 and the recording medium 24 is shown by the hatched area.

The AF error signal  $I_{AF}$  is given by

$$I_{AF} = (I_A + I_B + I_E + I_F + I_G + I_H + I_K + I_L) - (I_C + I_D + I_I + I_J)$$

where  $I_A, I_B, I_C, I_D, I_E, I_F, I_G, I_H, I_I, I_J, I_K$  and  $I_L$  are outputs from the photo-sensing areas.

For the photo-sensor having concentric photo-sensing areas as shown in FIG. 1C, the AF error signal  $I_{AF}$  is given by

$$I_{AF} = (I_A + I_B + I_E + I_F) - (I_C + I_D + I_G + I_H)$$

where  $I_A, I_B, I_C, I_D, I_E, I_F, I_G$  and  $I_H$  are outputs from the photo-sensing areas.

The AF error signal may be obtained by the operation for only one side of light beams. In the example of FIG. 1B,

$$I_{AF} = (I_A + I_B + I_E + I_F) - (I_C + I_D)$$

The principle of detection of the AT signal is now explained.

A groove having a depth of an approximately  $\frac{1}{8}$  of the wavelength is formed in a vicinity of the surface of the recording medium 24 and the signal is recorded or reproduced while the groove is used as a guide. A far field pattern formed by the light beam which is reflected by the groove and again passes through the object lens 23 changes with a positional relationship between the light spot and the groove. This is illustrated in FIGS. 11A, 11B and 11C. The upper part of FIGS. 11A, 11B and 11C show the positional relationship between the groove and the light spot, and the lower part shows an intensity distribution of the far field pattern.

For the split sensor shown in FIG. 1B, if the direction  $T-T'$  is aligned to the direction of the groove (the direction of the signal track), the AT error signal  $I_{AT}$  is given by

$$I_{AT} = (I_A + I_C + I_E + I_G + I_I + I_K) - (I_B + I_D + I_F + I_H + I_J + I_L)$$

For the split sensor shown in FIG. 1C,

$$I_{AT} = (I_A + I_C + I_E + I_G) - (I_B + I_D + I_F + I_H)$$

The AT error signal may also be obtained by the operation of the output of the photo-sensing areas which sense only one of the beams.

The differential detection of the information signal by the opto-magnetic method is now explained.

In FIGS. 12A and 12B, the X axis represents the direction of plane of polarization of the light beam directed to the recording medium 24, and the Y axis represents a direction orthogonal thereto.

The light beam reflected from the recording medium 24 has the polarization plane thereof inclined by a small angle  $\theta K$  by the magneto-optical effect as shown in FIG. 12A. This inclination is clockwise or counter-clockwise ( $\theta$  or  $-\theta K$ ) relative to a vertical direction of magnetic domain, and the angle is approximately  $1^\circ$ .

The light beam 121 reflected by the beam splitter 120 of FIG. 9 passes through the polarization element. If the transmission axis of the polarization element 122 is inclined approximately  $45^\circ$  with respect to the X axis, the following signal component in the intensity is produced in FIG. 12 depending on the inclination of the polarization plane:

$$S_1^2 \{ \cos(45^\circ - \theta K) \}^2 - \{ \cos(45^\circ + \theta K) \}^2$$

The second split beam 126 passes through the half-wave plate 123 before it passes through the polarization element 122. Accordingly, the polarization direction of the light beam 126 makes an angle of 90° with the light beam 121 as shown in FIG. 12B.

Accordingly, after it passed through the polarization element 122, the signal component in the intensity is

$$S_1'^2[\cos(45^\circ - \theta K)]^2 - [\cos(45^\circ + \theta K)]^2$$

The signal  $S_1'^2$  and  $S_1^2$  show only the P—P components for the sake of convenience. As seen from FIGS. 12A and 12B, the light beam 121 has a maximum signal amplitude and the light beam 126 has a minimum signal amplitude for the rotation of angle of  $\theta K$ .

When the rotation of the polarization plane is detected by the opto-magnetic signal by the arrangement shown in FIG. 9, the intensity modulation derived from the light beams 121 and 126 is reversed in phase. Accordingly, for FIG. 1B, the information signal  $I_S$  is given by

$$I_S = (I_A + I_B + I_C + I_D + I_E + I_F) - (I_G + I_H + I_I + I_J + I_K + I_L)$$

and, for FIG. 1C,

$$I_S = (I_A + I_B + I_C + I_D) - (I_E + I_F + I_G + I_H)$$

and the information signal is differentially detected.

To compare the arrangement of the present invention shown in FIG. 9 with the arrangement of the prior art, the arrangement is advantageous to reduce size and cost.

By integrating the optical elements shown in FIG. 9, the optical adjustment during assembly is facilitated, and misalignment of axes during use is prevented and a highly reliable optical pickup is provided. For example, in FIG. 13, the beam splitters 117 and 120, half-wave plate 123 and polarization element 122 are integrated by bonding material. In FIG. 14, the half-wave plate is arranged immediately behind the reflection plane of the beam splitter 120. In this case, parallelogram blocks 31 and 32 of the same size may be used and the preparation of the elements is simplified.

As shown in FIG. 15, a dielectric film or metal film 23 may be formed on the reflection plane 127 for the second light beam 126 to rotate the polarization plane instead of using the half-wave plate 123. In FIG. 16, a desired rotation angle is attained by a number of times of reflection when it is difficult to rotate the polarization plane by 90° by one reflection.

In order to detect the AF and AT error signals and the information signal, it is necessary to process the signals generated by the photo-sensing areas. Where the differential amplifier for such processing is incorporated in the photo-sensor together with the photo-sensing areas, signal detection which is resistive to external noise is attained.

FIG. 17 shows a third embodiment of the optical pickup of the present invention. The light beam emitted from the LD 26 is collimated by the collimator lens 21, reflected by the first beam splitter 117 and focused by the object lens 23 to a fine spot on the recording medium 24. The reflection beam from the recording medium 24 again passes through the object lens 23, passes through the first beam splitter 117 and the half-wave plate 123 with the direction of polarization plane being rotated by 45°, and is directed to the second beam

splitter 120 by which the beam is split into two beams. One split beam 121 reflected by the other beam splitter 120 is focused by the focusing lens 27 to the photo-sensor 28. On the other hand, the second split beam 126 is reflected by the reflection area 127 at the bottom of the beam splitter 120 and condensed by the condenser lens to the photo-sensor 28.

The photo-sensor 28 is arranged at a position spaced from a focal plane on which the split beams 121 and 126 are focused by the focusing lens 27. The photo-sensor 28 has twelve photo-sensing areas on the photo-sensing plane as shown in FIG. 1B.

The principle of the detection of the AF and AT error signals and the differential detection of the information signal in the arrangement of FIG. 17 applies equally to the second embodiment.

The differential detection of the information signal by the opto-magnetic method is now explained.

In FIG. 17, the reflection light from the recording medium 24 has the polarization plane thereof rotated by  $\theta K$  or  $-\theta K$  by the magnetic pattern (upward or downward orientation of magnetic domain) by the magneto-optical effect, and it is directed to the half-wave plate 123. The half-wave plate 123 has its crystal axis inclined to the incident plane of the beam splitter 120 by 22.5°. When the transmission and reflection characteristics of the beam splitter 120 are assumed as the polarization beam splitter characteristic (P component: 100% transmission, S component: 100% reflection), the transmitted and reflected light beams are detected by the photo-sensor as the signals having opposite phases, as shown in FIG. 18.

In FIG. 18, the X axis represents the reflection component of the polarization beam splitter, and the Y axis represents the transmission component. The light beam rotated by  $\theta K$  or  $-\theta K$  from the polarization plane of the incident light to the recording medium (the broken lines in FIG. 18 show the polarization plane) has its polarization plane rotated by 45° by the half-wave plate. Thereafter, it is reflected, transmitted and split by the polarization beam splitter 120. Thus, the two beams have the same variation amplitude ( $S_2'$ ,  $S_2$ ) and opposite phases. By detecting those two light beams using the photo-sensor 28, the information recorded on the recording medium can be read. In the photo-sensor of FIG. 1B, the opto-magnetic information signal  $I_S$  is given by

$$I_S = (I_A + I_B + I_C + I_D + I_E + I_F) - (I_G + I_H + I_I + I_J + I_K + I_L)$$

For the photo-sensor of FIG. 1C,

$$I_S = (I_A + I_B + I_C + I_D) - (I_E + I_F + I_G + I_H)$$

By integrating the optical elements of FIG. 17, the optical adjustment during the assembly is facilitated, misalignment of axes during use is prevented, and a highly reliable optical pickup is provided. For example, in FIG. 19, the beam splitter 117, half-wave plate 123 and beam splitter 120 are integrated by bonding material. In FIG. 20, the half-wave plate 123 is arranged immediately behind the reflection plane of the beam splitter 117. In this case, parallelogram blocks 130 and 131 of the same size may be used and the preparation of the elements is simplified.

In order to detect the AF and AT error signals and the information signal, it is necessary to process the signals generated by the photo-sensing areas. By incorporating the processing differential amplifier in the photo-sensor together with the photo-sensing areas, signal detection which is resistive to external noise is attained.

In the present embodiment, the variation of the signals generated by the photo-sensing areas of the sensor is detected to improve the precision.

The advantage of the differential detection is explained with reference to a third embodiment. FIGS. 21A and 21B show signal amplitudes generated by the sensing areas of the sensor. The light beam reflected by the recording medium 24 having a longitudinal axis along the polarization direction of the incident light beam has its polarization plane rotated by  $\theta K$  or  $-\theta K$  depending on the orientation (up or down) of the axis of the opto-magnetic pattern. Since the combination of the half-wave plate 123 and the polarization beam splitter 120 is equivalent to a system having a polarization plate whose transmission axis is inclined by  $45^\circ$ , difference  $S_1$  and  $S'_1$  of the projection component to a virtual transmission axis (broken line axis inclined by  $45^\circ$ ) are signal amplitudes. Since  $\theta K$  and  $-\theta K$  vary with time depending on the opto-magnetic pattern, the signal intensity changes are represented by the light beams shown in FIGS. 22A and 22B, which are shifted by  $180^\circ$  in phase from each other. The opto-magnetic signal generated by the sensing areas of the photo-sensor is reversed in phase but noise components (noise from the recording medium and swing noise of the LD light) usually ride on those signals and the noise components are of the same phase.

Accordingly, when the signals from the sensing areas of the sensor are differentially detected, the signal components are added and the noise components are cancelled. If the optical system is precisely arranged, the signal components  $S_1^2$  and  $S'_1^2$  from the respective sensors are equal and the noise amplitude are also equal. Accordingly, the signal is doubled and the noise is cancelled. Thus, the differential detection provides a high S/N signal.

As described hereinabove, in accordance with the present invention, the light beam from the recording medium is split and they are differentially detected by the single photo-detector having the split photo-sensing plane. Accordingly,

1. The optical pickup can be constructed in a compact size.
2. The S/N ratio of the signal detection is improved by the differential detection.
3. The number of components is reduced and the cost is reduced.
4. By integrating the components, a more reliable pickup is provided.
5. Because only one photo-sensor is used, no consideration of the variation of the characteristics between the sensors is required, and the position adjustment is simple.
6. By arranging the signal processing circuit on the same chip as the photo-detector, signal detection which is resistive to external noise is attained.

We claim:

1. An optical pickup apparatus for reproducing information magnetically recorded on a recording medium, comprising:

a light source for generating a light beam; an object lens for focusing the light beam generated from said light source onto the recording medium, on which the light beam is polarized in a predetermined direction; a beam splitter arranged in an optical path extending from said light source to the recording medium, said beam splitter having a reflection plane for reflecting the light beam from said light source toward the recording medium, and for simultaneously causing the reflected light from the recording medium to pass through said reflection plane to separate the reflected light beam from the light beam irradiated toward the recording medium, a polarization direction of the reflected light beam being rotated through a predetermined angle in accordance with the recorded information, said beam splitter splitting the reflected light beam passed through said reflection plane into first and second light beams both of which are polarized in directions perpendicular to each other, said beam splitter comprising a crystal having a bi-refractive property;

first and second detection means for detecting said first and second light beams respectively, and for providing first and second detection outputs respectively corresponding thereto; and means for differentiating the detection outputs from said detection means so as to provide information signals.

2. An apparatus according to claim 1, wherein said first and second detection means comprise two photo-sensing planes of a photo-detector formed on a single substrate.

3. An optical pickup apparatus, comprising: polarized beam irradiating means for irradiating an optical information recording medium with a light beam polarized in a predetermined direction; a beam splitter including a reflection plane for reflecting the light beam from said irradiating means toward the recording medium and for causing the reflected light from the recording medium to pass therethrough to separate the reflected light beam from the light beam irradiated toward the recording medium, and a prism comprising a crystal having a birefringence property, which is arranged in an optical path separated in an optical path of the light beam irradiated toward the recording medium, in an optical path of the reflected light beam from the recording medium and which comes in contact with said reflection plane, wherein said prism splits the light beam passed through said reflection plane into first and second light beams both of which are polarized in directions perpendicular to each other by causing travelling directions of the first and second light beams to be different from each other; and

first and second detection means for detecting said first and second light beams, respectively, and for providing first and second detection outputs respectively corresponding thereto.

4. An apparatus according to claim 3, wherein said first and second detection means comprise two photo-sensing planes of a photo-detector formed on a single substrate.

\* \* \* \* \*

UNITED STATES PATENT AND TRADEMARK OFFICE  
CERTIFICATE OF CORRECTION

PATENT NO. : 5,416,755  
DATED : May 16, 1995  
INVENTOR(S) : KIYONOBU ENDO, ET AL.

Page 1 of 2

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

COLUMN 1

Line 57, "a" (first occurrence) should be deleted.

COLUMN 2

Line 18, "and FIG. 23" should read --and ¶ FIG. 23--.

COLUMN 3

Line 17, "compound of the" should be deleted.

Line 18, "first" should read --first compound of the--.

COLUMN 4

Line 37, "embodiment" should read --embodiments--.

Line 48, "splitter 22" should read --splitter 22'--.

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UNITED STATES PATENT AND TRADEMARK OFFICE  
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PATENT NO. : 5,416,755  
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Page 2 of 2

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

COLUMN 7

Line 46, "23" should read --23'--.

Signed and Sealed this

Twenty-second Day of August, 1995

Attest:



BRUCE LEHMAN

Attesting Officer

Commissioner of Patents and Trademarks